

# Study on the effect and mechanism of zirconia on the sinterability of yttria transparent ceramic

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## Abstract

Transparent  $Y_2O_3$  ceramics were fabricated by solid-state reaction using high purity  $Y_2O_3$  and  $ZrO_2$  powder as starting material. The results indicated that  $ZrO_2$  additive can improve the transparency of  $Y_2O_3$  ceramic greatly. The best transmittance appears with 3 at.%  $ZrO_2$  doped  $Y_2O_3$  transparent ceramic with transmittance at 1100 nm of 83.1%, which is up to 98.6% of the theoretical value. The microstructure is uniform and no secondary phase is observed in the ceramic with the average grain size of 15  $\mu m$ . The mechanism of  $ZrO_2$  improving the transparency of  $Y_2O_3$  ceramic is analyzed in detail. On this basis,  $Yb^{3+}$  doped  $Y_2O_3$  transparent ceramic was also fabricated and spectroscopic properties were investigated.

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**Keywords:**  $Y_2O_3$ ; Transparent ceramics; Optical properties; Sintering

## 1. Introduction

Since the first laser demonstration on Nd:YAG polycrystalline ceramic in 1995,<sup>1</sup> more and more researches are focused on transparent ceramic laser materials.<sup>2,3</sup> Much progress has been made in improving the optical quality of ceramic as well as in exploring new laser materials.

$Y_2O_3$  is promising laser host material for trivalent lanthanide activators due to its superior properties such as refractory nature, stability, and optical clarity over a broad spectral range.<sup>4</sup> However,  $Y_2O_3$  crystal is extremely difficult to fabricate because of high melting point (2430 °C) and phase transformation from cubic phase to high-temperature hexagonal phase at 2350 °C. Instead, transparent  $Y_2O_3$  ceramic is easily prepared at low sintering temperature.

Conventionally,  $Y_2O_3$  transparent ceramic has been fabricated by hot press or normal sintering with  $ThO_2$ ,  $HfO_2$  and  $La_2O_3$  as additives.<sup>5,6</sup> However, these additives were not widely

used for toxicity and high expense. In recent years, many methods have been studied to fabricate  $Y_2O_3$  nanopowders which were finally sintered to transparent ceramic.<sup>7,8</sup> Unfortunately, most of these methods involve complicated steps and exposing in air for a long time, the transparency of ceramic is prone to decrease due to the pollution. Although  $Y_2O_3$  transparent ceramic have been studied widely,  $ZrO_2$  used as additive is less known to the best of our knowledge.<sup>9</sup> In this study,  $ZrO_2$  was introduced as additive and  $Y_2O_3$  transparent ceramics were sintered in vacuum. The effect of  $ZrO_2$  on the sinterability of the ceramic was investigated systematically to obtain the optimum  $ZrO_2$  doping concentration. On this basis,  $Yb^{3+}$  doped  $Y_2O_3$  transparent ceramic was fabricated and the spectral properties were demonstrated.

## 2. Experimental

$Y_2O_3$  (99.999%, Changchun Ruipu Rare-Materials Co. Ltd., Changchun, China) and  $ZrO_2$  (99.99%, Sinopharm Chemical Reagent Co. Ltd., Shanghai, China) with a manufacturer-determined particle size of 1  $\mu m$  were used as starting materials. According to the formula of  $(Y_{1.0-x}Zr_x)_2O_3$  ( $x=0-0.10$ ), the powders were blended and ball milled in absolute ethyl alco-

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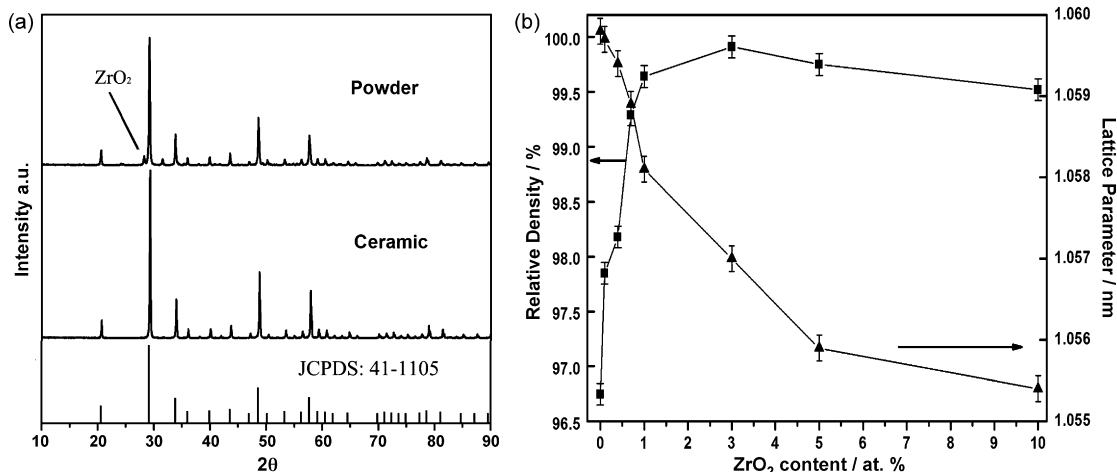


Fig. 1. (a) XRD patterns of 3 at.%  $ZrO_2$  doped  $Y_2O_3$  powder and sintered ceramic and (b) change of relative density and lattice parameter with  $ZrO_2$  content.

hol for 24 h with agate balls. After dried at  $130^\circ C$  overnight, the powder mixture was crushed and sieved through 200-mesh screen. Disks with 20 mm in diameter were compacted in steel mold at 15 MPa and then isostatically pressed at 250 MPa. Sintering was conducted at  $1800^\circ C$  for 15 h in vacuum.

The structure of ceramic was determined by X-ray diffraction (XRD, Cu target, Model Ultima IV, Rigaku, Japan). The specimens (1.0 mm thick) were polished on both sides to measure optical transmittance with JASCO V-900 UV/VIS/NIR spectrophotometer. JSM 6360-LA scanning electron microscope (SEM) and energy-dispersive spectroscopy (EDS) were used to analyse the microstructure and component of the ceramics. Sintered density was measured by Archimedes' Principle. The fluorescence spectrum was acquired by a TRIAX 550 spectrophotometer with InGaAs LD as the pump source (excited at 940 nm).

### 3. Results

Fig. 1(a) shows XRD patterns of the powder and sintered ceramic. It was observed that except diffraction peaks of  $Y_2O_3$ , the diffraction peak corresponding to  $ZrO_2$  was also detected in the milled powder. After sintered, the peak corresponding to  $ZrO_2$  disappeared and the samples were well crystallized and coincided with cubic  $Y_2O_3$  phase ( $Y_2O_3$ , JCPDS41-1105). The lattice parameter and relative density of these ceramics were calculated and shown in Fig. 1(b). The lattice parameter decreases with the increase of  $ZrO_2$  content, which is mainly due to the smaller radius of  $Zr^{4+}$  ( $R=0.80 \text{ \AA}$ ) compared with  $Y^{3+}$  ( $R=0.90 \text{ \AA}$ ). The relative density increases rapidly with the content of  $ZrO_2$ , and the highest relative density is 99.91% for 3.0 at.%  $ZrO_2$  doped transparent ceramic. It can be concluded that  $ZrO_2$  can greatly increase the sintered density which is one of the definitive factors of transparency.

The photographs of  $Y_2O_3$  ceramics with different concentration of  $ZrO_2$  are provided in Fig. 2, which demonstrates that the addition of  $ZrO_2$  improves the transmittance of  $Y_2O_3$  ceramic to a great extent.

The microstructure of the polished surface was investigated after etched in  $H_3PO_4$  for 3 min at  $85^\circ C$ . As shown in Fig. 3(a), The microstructure of 3.0 at.%  $ZrO_2$  doped  $Y_2O_3$  ceramic was uniform and the grain size was comparatively homogeneous without abnormal grain growth. The grain size was measured by the grain size calculation software attached to the SEM and a mean linear intercept method, and the mean grain size was found to be  $15 \mu m$  by averaging over 200 grains. The grain boundary is clear without pores or impurities. With  $ZrO_2$  content increasing to 10.0 at.%, secondary phase was observed on the grain boundary as shown in Fig. 3(b). According to the EDS analysis, the mole ratio of Zr and Y elements is 13: 87 which is larger than the designed value of 10:90. It could be deduced that a fraction of  $ZrO_2$  separated out from  $Y_2O_3$ - $ZrO_2$  solid solution and formed a secondary phase.

Fig. 4 presents the optical transmittance of  $Y_2O_3$  transparent ceramics doped with different  $ZrO_2$  content. With the increasing of  $ZrO_2$  concentration, the transmittance increased and then gradually decreased. Using  $ZrO_2$  as a dopant, the refractive index of  $ZrO_2$  doped  $Y_2O_3$  ceramic will slightly change and so is the theoretical transmission. We measured the refractive index of 3.0 at.%  $ZrO_2$  doped  $Y_2O_3$  ceramic as 1.82. The theoretical transmittance accurately calculated from the refractive index is

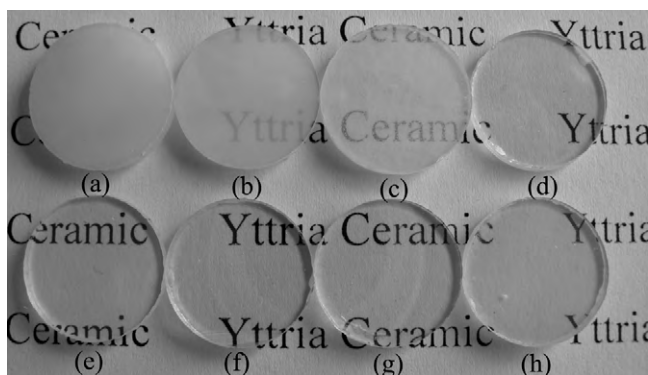


Fig. 2. Photographs of  $Y_2O_3$  ceramics with different  $ZrO_2$  content (a) 0, (b) 0.1 at.%, (c) 0.4 at.%, (d) 0.7 at.%, (e) 1.0 at.%, (f) 3.0 at.%, (g) 5.0 at.%, (h) 10.0 at.%.

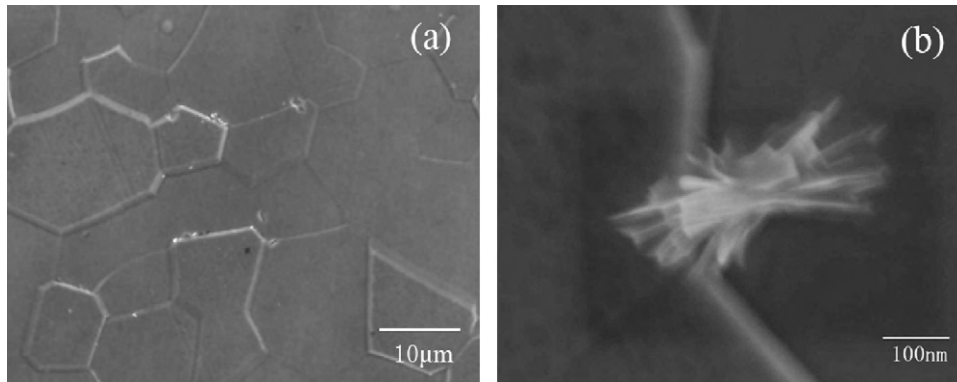


Fig. 3. Microstructure of  $\text{Y}_2\text{O}_3$  transparent ceramics vacuum sintered at  $1800^\circ\text{C}$  for 15 h (a)  $(\text{Y}_{0.97}\text{Zr}_{0.03})_2\text{O}_3$  solid solution (b)  $\text{Y}_2\text{O}_3$ –10 at.% $\text{ZrO}_2$  two phase alloy.

84.3%.<sup>10</sup> The optimum result occurs with 3.0 at.%  $\text{ZrO}_2$  and the transmittance at 1100 nm is 83.1%, which is up to 98.6% of the theoretical value. It can be seen from the phase diagram that the solid solution limit of  $\text{ZrO}_2$  in  $\text{Y}_2\text{O}_3$  is about 4.0 at.% at  $1800^\circ\text{C}$ .<sup>11</sup> Alloy with 3.0 at.%  $\text{ZrO}_2$  doped content was close to the solid solution limit and increase point defects to the extreme, which benefits for the elimination of pores and ceramic densification. However, increase in the  $\text{ZrO}_2$  content beyond the solid solution limit, may lead to the precipitation of a secondary phase (Fig. 3(b)), which would cause the scattering of light in ceramic body and decrease the transparency.

After the optimum concentration of  $\text{ZrO}_2$  (3.0 at.%) was obtained, 5.0 at.%  $\text{Yb}^{3+}$  doped  $\text{Y}_2\text{O}_3$  transparent ceramic was obtained after sintering at  $1800^\circ\text{C}$  for 15 h. The transmittance, absorption and emission spectra are given in Fig. 5. The samples demonstrates high transmittance not only in near infrared but also in visible region, as shown in Fig. 5(a), which indicates the sintered ceramics have high quality without scattering centers. From Fig. 5(b), we can see that the  $\text{Yb}:\text{Y}_2\text{O}_3$  has a strong and broad absorption band around 950 nm, which matches well with the emission wavelength of InGaAs laser diodes. The absorption cross-section of  $\text{Yb}^{3+}$  can be calculated by Lambert' Law<sup>12</sup>:

$$\sigma_{abs} = \frac{\alpha}{C} \quad (1)$$

where  $\alpha$  is the absorption coefficient,  $C$  is the concentration of  $\text{Yb}^{3+}$  ions. The absorption cross-sections at 947 nm and 973 nm are  $0.959 \times 10^{-20}$  and  $1.175 \times 10^{-20} \text{ cm}^2$ , respectively, both of them are larger than that of  $\text{Yb}^{3+}$  doped yttrium lanthanum oxide transparent ceramic reported in Ref. [13]. Three emission peaks corresponding to the transition of  ${}^2\text{F}_{5/2} \rightarrow {}^2\text{F}_{7/2}$  centered at 977 nm, 1032 nm and 1075 nm. Among them, the strongest peak is at 1032 nm with FWHM of 17 nm. The broad FWHM may play an active role in obtaining ultrashort pulse or femtosecond laser. Laser experiments will be reported in the near future.

#### 4. Discussion

It was also reported that the transparent  $\text{Y}_2\text{O}_3$  ceramic can be obtained without additive using  $\text{Y}_2\text{O}_3$  nanopowder as raw material.<sup>7</sup> Nanopowder possesses narrow size distribution and high surface activity, which is beneficial for the sintering and transparency. As commercial powder was used in our experiment, due to the large size and poor dispersibility of the powder, transparency cannot be achieved without the addition of  $\text{ZrO}_2$ .

Combined with sintering kinetics, thermodynamics and experimental results above, the mechanism of  $\text{ZrO}_2$  in improving the transparency of  $\text{Y}_2\text{O}_3$  ceramic can be visualized as follows:

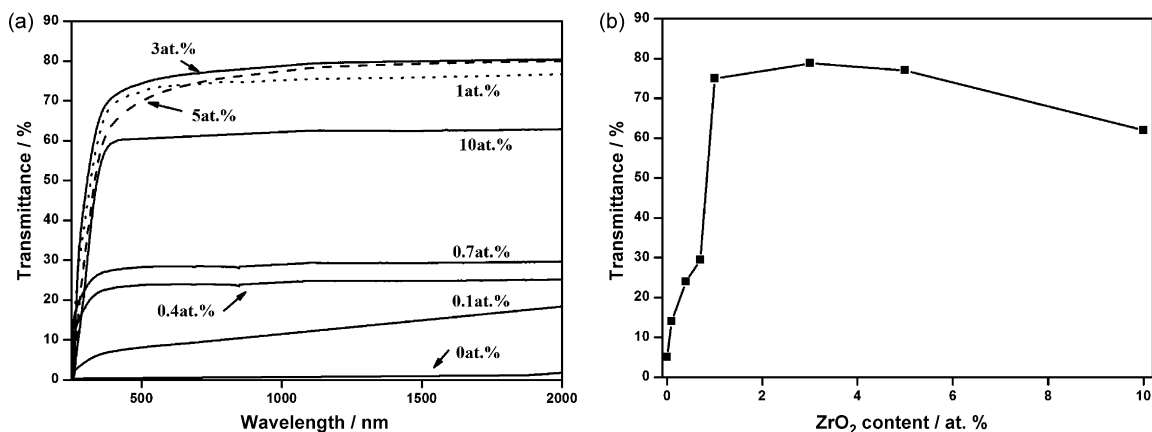


Fig. 4. Transmittance of  $\text{Y}_2\text{O}_3$  transparent ceramics: (a) the transmittance spectra of  $\text{Y}_2\text{O}_3$  transparent ceramics with different  $\text{ZrO}_2$  content and (b) the change of transmittance at 1100 nm with the  $\text{ZrO}_2$  content.

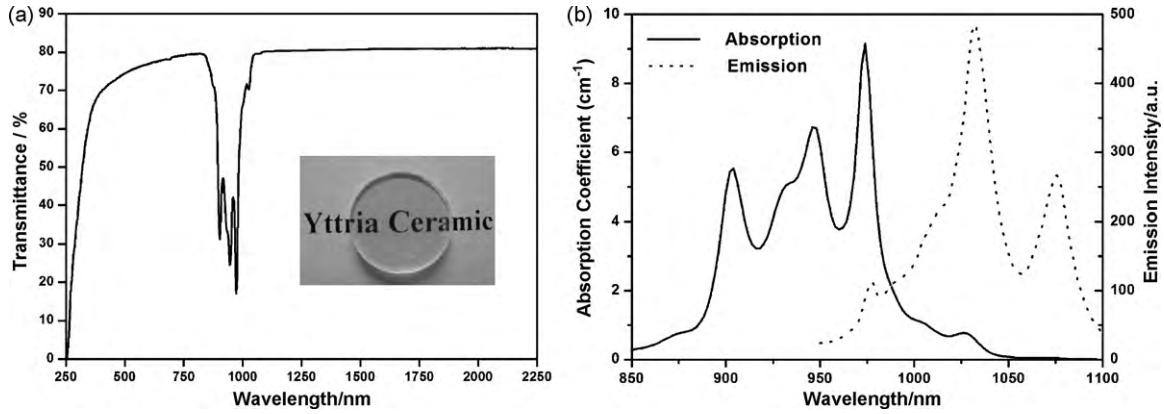


Fig. 5. (a) Transmittance spectra of  $(\text{Yb}_{0.05}\text{Y}_{0.92}\text{Zr}_{0.03})_2\text{O}_3$  transparent ceramic and (b) absorption and emission spectra of  $(\text{Yb}_{0.05}\text{Y}_{0.92}\text{Zr}_{0.03})_2\text{O}_3$  transparent ceramic.

- (1) The addition of  $\text{ZrO}_2$  decreases the melting point of  $\text{ZrO}_2\text{--Y}_2\text{O}_3$  binary system,<sup>11</sup> and so is the sintering temperature.
- (2) The radius of  $\text{Zr}^{4+}$  ( $R=0.80 \text{ \AA}$ ) is similar with that of  $\text{Y}^{3+}$  ( $R=0.90 \text{ \AA}$ ), which ensures small lattice distortion as  $\text{Zr}^{4+}$  substituting for  $\text{Y}^{3+}$ .
- (3) In the final stage of sintering, a fraction of grains with low surface energy tend to grow to larger size on the consumption of surrounding smaller grains, which is known as discontinuous or exaggerated grain growth. During this process, owing to the high mobility of grain boundary, pores are easily embraced in the grains and cause the decrease of transparency.  $\text{ZrO}_2$  is prone to form solid solution on the grain boundaries owing to its high melting point ( $2715 \text{ }^\circ\text{C}$ ), which can hamper with the grain boundary mobility and occurrence of secondary recrystallization due to the solute drag mechanism. This benefits the elimination of pores and the uniformity of grain sizes, both of which are absolutely critical to transmittance.
- (4) The sintering technology of transparent ceramic is different from that of ordinary ceramic which aims to increase sintering rate and shorten production period. However, for transparent ceramic, high sintering rate may result in closed porosity inside grains which is difficult to remove during sintering and cause the decreasing of the transparency. Indeed, it is known that the diffusion coefficient of oxygen anion is much higher than that of yttrium cation in pure  $\text{Y}_2\text{O}_3$ .<sup>14</sup> So cation diffusion is the rate-controlling step for grain boundary migration. Pei-Lin Chen also reported that the diffusion of  $[\text{Y}_i^{\bullet\bullet\bullet}]$  dominates the grain boundary mobility.<sup>15</sup> We estimate the defect concentration in  $\text{Y}_2\text{O}_3$  as follows:

Schottky defect:



Frenkel defect:



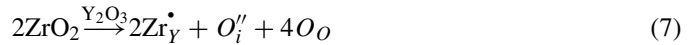
The relationship between  $\text{V}_Y^{\bullet\bullet\bullet}$ ,  $\text{Y}_i^{\bullet\bullet\bullet}$  and  $\text{O}_i^{\bullet\bullet}$  is deduced as:

$$[\text{V}_Y^{\bullet\bullet\bullet}] = [\text{O}_i^{\bullet\bullet}]^{1.5} \left( \frac{K_S^{0.5}}{K_F^{1.5}} \right) \exp \left[ -\frac{\Delta G_S - 3\Delta G_F^A}{2kT} \right] \quad (5)$$

$$[\text{Y}_i^{\bullet\bullet\bullet}] = [\text{O}_i^{\bullet\bullet}]^{-1.5} \left( \frac{K_F K_F^{1.5}}{K_S^{0.5}} \right) \exp \left[ -\frac{2\Delta G_F - \Delta G_S + 3\Delta G_F^A}{2kT} \right] \quad (6)$$

In the above,  $K_S$ ,  $K_F^A$  and  $K_F$  are the pre-exponential temperature-independent.  $\Delta G_S$ ,  $\Delta G_F^A$  and  $\Delta G_F$  are formation free energy of Schottky and Frenkel defect.

After  $\text{ZrO}_2$  doping, the defect reaction is as follows:



It can be concluded by the above formula that every two  $\text{Zr}^{4+}$  create one  $\text{O}_i^{\bullet\bullet}$ , so that  $[\text{V}_Y^{\bullet\bullet\bullet}]$  is increased but  $[\text{Y}_i^{\bullet\bullet\bullet}]$  is decreased. The decreasing of  $[\text{Y}_i^{\bullet\bullet\bullet}]$  concentration results in the slowdown of grain boundary mobility and sintering rate, which ensure the expelling of pores and densification of ceramic. The average grain size of  $\text{ZrO}_2$  doped ceramic is  $15 \mu\text{m}$ , which is much smaller than  $50 \mu\text{m}$  reported in Ref. [2]. This also confirms that the addition of  $\text{ZrO}_2$  decreases grain boundary mobility. Meantime, 3 at. %  $\text{ZrO}_2$  doped sample lead the point defects to a appropriate amount. It is not only benefit for the expelling of pores, but also not too much to cause grey darkening which will bring decreasing of the transmittance in the visible range.<sup>16</sup>

## 5. Conclusion

$\text{Y}_2\text{O}_3$  transparent ceramics were fabricated by vacuum sintering technique with  $\text{ZrO}_2$  as additive. 3 at. %  $\text{ZrO}_2$  doped  $\text{Y}_2\text{O}_3$  transparent ceramics had the best transmittance with the transmittance of 83.1% at 1100 nm. The microstructure is uniform and no secondary phase is observed in the ceramics with average grain size of  $15 \mu\text{m}$ . The results showed that the introduction of  $\text{ZrO}_2$  improves the transmittance of  $\text{Y}_2\text{O}_3$  ceramic greatly and the mechanism of  $\text{ZrO}_2$  improving the transparency of  $\text{Y}_2\text{O}_3$

ceramic is analyzed in detail. With  $\text{ZrO}_2$  as additive, 5.0 at.%  $\text{Yb}^{3+}$  doped  $\text{Y}_2\text{O}_3$  transparent ceramic was also prepared. The absorption cross-sections at 947 nm ( $\sigma_{\text{abs}} = 0.959 \times 10^{-20} \text{ cm}^2$ ) and 973 nm ( $\sigma_{\text{abs}} = 1.175 \times 10^{-20} \text{ cm}^2$ ) are larger than that of  $\text{Yb}^{3+}$  doped yttrium lanthanum oxide transparent ceramic.

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